

§ core region --- perturbation method

(1) characteristic velocity

$$u_c^* = \frac{g\beta\Delta TH^3}{vL} = \frac{\alpha}{L} Ra_H \quad \text{and} \quad v_c^* = u_c^* \frac{H}{L} = \varepsilon^{1/2} \cdot \frac{\alpha}{L} Ra_H, \text{ with } \varepsilon \equiv \left(\frac{H}{L} \right)^2$$

(2) Nondimensionalize

$$u \mapsto u/u_c^* = \frac{uL}{\alpha} Ra_H^{-1} \quad \text{and} \quad v \mapsto v/v_c^* = \varepsilon^{-1/2} \cdot \frac{v\alpha}{L} Ra_H^{-1}$$

$$x \mapsto x/L \quad \text{and} \quad y \mapsto y/H$$

$$T \mapsto \frac{T - T_{cold}}{\Delta T} \quad \text{such that} \quad T(x=0) = 0 \quad \text{and} \quad T(x=L) = 1$$

(3) Dimensional equations

$$\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} = 0$$

$$\underbrace{\frac{\partial}{\partial x} \left(u \frac{\partial v}{\partial x} + v \frac{\partial v}{\partial y} \right)}_{u \frac{\partial T}{\partial x} + v \frac{\partial T}{\partial y}} - \underbrace{\frac{\partial}{\partial y} \left(u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} \right)}_{u \frac{\partial^2 T}{\partial x^2} + v \frac{\partial^2 T}{\partial y^2}} = v \left\{ \frac{\partial}{\partial x} \left(\frac{\partial^2 v}{\partial x^2} + \frac{\partial^2 v}{\partial y^2} \right) - \frac{\partial}{\partial y} \left(\frac{\partial^2 u}{\partial x^2} + \frac{\partial^2 u}{\partial y^2} \right) \right\} + g\beta \frac{\partial T}{\partial x}$$

$$u \frac{\partial T}{\partial x} + v \frac{\partial T}{\partial y} = \alpha \left\{ \frac{\partial^2 T}{\partial x^2} + \frac{\partial^2 T}{\partial y^2} \right\}$$

(4) Dimensionless equations:

$$(a) \underbrace{\frac{u_c^*}{L} \frac{\partial u}{\partial x} + \frac{v_c^*}{H} \frac{\partial v}{\partial y} = 0}_{\underline{u_c^* v_c^* / L^2}} \Rightarrow \frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} = 0$$

$$(b) \underbrace{\frac{\partial}{\partial x} \left(u \frac{\partial v}{\partial x} + v \frac{\partial v}{\partial y} \right)}_{\frac{u_c^* v_c^*}{L^2}} - \underbrace{\frac{\partial}{\partial y} \left(u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} \right)}_{\frac{u_c^*}{LH}} = v \left\{ \frac{\partial}{\partial x} \left(\frac{\partial^2 v}{\partial x^2} + \frac{\partial^2 v}{\partial y^2} \right) - \frac{\partial}{\partial y} \left(\frac{\partial^2 u}{\partial x^2} + \frac{\partial^2 u}{\partial y^2} \right) \right\} + \underbrace{g\beta \frac{\partial T}{\partial x}}_{\frac{g\beta\Delta T}{L}}$$

$$\bullet \frac{u_c^* v_c^* / L^2}{u_c^* / LH} = \frac{v_c^*}{u_c^*} \cdot \frac{H}{L} = \varepsilon$$

$$\bullet \frac{v v_c^* / L^3}{u_c^* / LH} = \frac{\varepsilon^{1/2}}{u_c^*} \cdot \frac{vH}{L^2} = \varepsilon^{1/2} \frac{L}{\alpha} Ra_H^{-1} \cdot \frac{vH}{L^2} = \varepsilon \Pr Ra_H^{-1}$$

- $\frac{vv_c^*/LH^2}{u_c^{*2}/LH} = \frac{\varepsilon^{1/2}}{u_c^*} \cdot \frac{v}{H} = \varepsilon^{1/2} \frac{L}{\alpha} Ra_H^{-1} \cdot \frac{v}{H} = \Pr Ra_H^{-1}$
- $\frac{vu_c^*/HL^2}{u_c^{*2}/LH} = \frac{1}{u_c^*} \cdot \frac{v}{L} = \frac{L}{\alpha} Ra_H^{-1} \cdot \frac{v}{L} = \Pr Ra_H^{-1}$
- $\frac{vu_c^*/H^3}{u_c^{*2}/LH} = \frac{1}{u_c^*} \cdot \frac{vL}{H^2} = \frac{L}{\alpha} Ra_H^{-1} \cdot \frac{vL}{H^2} = \varepsilon^{-1} \Pr Ra_H^{-1}$
- $\frac{g\beta\Delta T/L}{u_c^{*2}/LH} = \left(\frac{vL}{g\beta\Delta TH^3} \right)^2 \cdot \frac{g\beta\Delta TH}{1} = \frac{v^2 L^2}{g\beta\Delta TH^5} = \frac{\alpha v}{g\beta\Delta TH^3} \cdot \frac{v}{\alpha} \cdot \frac{L^2}{H^2} = \varepsilon^{-1} \Pr Ra_H^{-1}$

Therefore

$$\frac{Ra_H}{\Pr} \left\{ \varepsilon \frac{\partial}{\partial x} \left(u \frac{\partial v}{\partial x} + v \frac{\partial v}{\partial y} \right) - \frac{\partial}{\partial y} \left(u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} \right) \right\} = \left\{ \frac{\partial}{\partial x} \left(\varepsilon \frac{\partial^2 v}{\partial x^2} + \frac{\partial^2 v}{\partial y^2} \right) - \frac{\partial}{\partial y} \left(\frac{\partial^2 u}{\partial x^2} + \varepsilon^{-1} \frac{\partial^2 u}{\partial y^2} \right) \right\} + \varepsilon^{-1} \frac{\partial T}{\partial x}$$

or

$$\varepsilon \frac{Ra_H}{\Pr} \left\{ \varepsilon \frac{\partial}{\partial x} \left(u \frac{\partial v}{\partial x} + v \frac{\partial v}{\partial y} \right) - \frac{\partial}{\partial y} \left(u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} \right) \right\} = \varepsilon \frac{\partial}{\partial x} \left(\varepsilon \frac{\partial^2 v}{\partial x^2} + \frac{\partial^2 v}{\partial y^2} \right) - \frac{\partial}{\partial y} \left(\varepsilon \frac{\partial^2 u}{\partial x^2} + \frac{\partial^2 u}{\partial y^2} \right) + \frac{\partial T}{\partial x}$$

$$(c) \quad \underbrace{u \frac{\partial T}{\partial x}}_{\frac{u_c^*\Delta T}{L}} + \underbrace{v \frac{\partial T}{\partial y}}_{\frac{v_c^*\Delta T}{H}} = \alpha \left\{ \frac{\partial^2 T}{\partial x^2} + \frac{\partial^2 T}{\partial y^2} \right\} \\ \frac{\alpha\Delta T}{L^2} \quad \frac{\alpha\Delta T}{H^2}$$

$$\text{■ } \frac{u_c^*\Delta T/L}{\alpha\Delta T/H^2} = \frac{\alpha}{L} Ra_H \frac{H^2}{\alpha L} = \varepsilon Ra_H$$

$$\text{■ } \frac{v_c^*\Delta T/H}{\alpha\Delta T/H^2} = \varepsilon^{1/2} \frac{\alpha}{L} Ra_H \frac{H}{\alpha} = \varepsilon Ra_H$$

$$\frac{\alpha \Delta T / L^2}{\alpha \Delta T / H^2} = \frac{H^2}{L^2} = \varepsilon$$

Therefore

$$\varepsilon Ra_H \left\{ u \frac{\partial T}{\partial x} + v \frac{\partial T}{\partial y} \right\} = \varepsilon \frac{\partial^2 T}{\partial x^2} + \frac{\partial^2 T}{\partial y^2}$$

(5) perturbation solution

$$(u, v, T) = (u_0, v_0, T_0) + \varepsilon(u_1, v_1, T_1) + \varepsilon^2(u_2, v_2, T_2) + \dots$$

Substitute into dimensionless equations:

$$(a) \quad \frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} = 0 \Rightarrow \left(\frac{\partial u_0}{\partial x} + \frac{\partial v_0}{\partial y} \right) + \varepsilon \left(\frac{\partial u_1}{\partial x} + \frac{\partial v_1}{\partial y} \right) + \varepsilon^2 \left(\frac{\partial u_2}{\partial x} + \frac{\partial v_2}{\partial y} \right) + \dots$$

(b)

$$\begin{aligned} \varepsilon \frac{Ra_H}{Pr} \left\{ \varepsilon \frac{\partial}{\partial x} \left(u \frac{\partial v}{\partial x} + v \frac{\partial v}{\partial y} \right) - \frac{\partial}{\partial y} \left(u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} \right) \right\} &= \varepsilon \frac{\partial}{\partial x} \left(\varepsilon \frac{\partial^2 v}{\partial x^2} + \frac{\partial^2 v}{\partial y^2} \right) - \frac{\partial}{\partial y} \left(\varepsilon \frac{\partial^2 u}{\partial x^2} + \frac{\partial^2 u}{\partial y^2} \right) + \frac{\partial T}{\partial x} \\ &\Downarrow \\ -\varepsilon \frac{Ra_H}{Pr} \frac{\partial}{\partial y} \left(u_0 \frac{\partial u_0}{\partial x} + v_0 \frac{\partial u_0}{\partial y} \right) + \varepsilon^2 \frac{Ra_H}{Pr} \left\{ \frac{\partial}{\partial x} \left(u_0 \frac{\partial v_0}{\partial x} + v_0 \frac{\partial v_0}{\partial y} \right) - \frac{\partial}{\partial y} \left(u_1 \frac{\partial u_0}{\partial x} + v_1 \frac{\partial u_0}{\partial y} + u_0 \frac{\partial u_1}{\partial x} + v_0 \frac{\partial u_1}{\partial y} \right) \right\} \\ + \dots &= -\frac{\partial^3 u_0}{\partial y^3} + \frac{\partial T_0}{\partial x} + \varepsilon \left\{ \frac{\partial^3 v_0}{\partial x \partial y^2} - \frac{\partial^3 u_0}{\partial y \partial x^2} - \frac{\partial^3 u_1}{\partial y^3} + \frac{\partial T_1}{\partial x} \right\} + \varepsilon^2 \left\{ \frac{\partial^3 v_0}{\partial x^3} + \frac{\partial^3 v_1}{\partial x \partial y^2} - \frac{\partial^3 u_1}{\partial y \partial x^2} - \frac{\partial^3 u_2}{\partial y^3} + \frac{\partial T_2}{\partial x} \right\} + \dots \end{aligned}$$

(c)

$$\varepsilon Ra_H \left\{ u \frac{\partial T}{\partial x} + v \frac{\partial T}{\partial y} \right\} = \varepsilon \frac{\partial^2 T}{\partial x^2} + \frac{\partial^2 T}{\partial y^2}$$

\Downarrow

$$\varepsilon Ra_H \left\{ u_0 \frac{\partial T_0}{\partial x} + v_0 \frac{\partial T_0}{\partial y} \right\} + \varepsilon^2 Ra_H \left\{ u_0 \frac{\partial T_1}{\partial x} + v_0 \frac{\partial T_1}{\partial y} + u_1 \frac{\partial T_0}{\partial x} + v_1 \frac{\partial T_0}{\partial y} \right\} + \dots$$

$$= \frac{\partial^2 T_0}{\partial y^2} + \varepsilon \left(\frac{\partial^2 T_0}{\partial x^2} + \frac{\partial^2 T_1}{\partial y^2} \right) + \varepsilon^2 \left(\frac{\partial^2 T_1}{\partial x^2} + \frac{\partial^2 T_2}{\partial y^2} \right) + \dots$$

(6) Terms multiplied by the same power of ε are grouped together and set equal to zero:

(a) ε^0 :

$$\frac{\partial u_0}{\partial x} + \frac{\partial v_0}{\partial y} = 0 \quad (1)$$

$$-\frac{\partial^3 u_0}{\partial y^3} + \frac{\partial T_0}{\partial x} = 0 \quad (2)$$

$$\frac{\partial^2 T_0}{\partial y^2} = 0 \quad (3)$$

(b) ε^1 :

$$\frac{\partial u_1}{\partial x} + \frac{\partial v_1}{\partial y} = 0 \quad (1)$$

$$-\frac{Ra_H}{Pr} \frac{\partial}{\partial y} \left(u_0 \frac{\partial u_0}{\partial x} + v_0 \frac{\partial u_0}{\partial y} \right) = \frac{\partial^3 v_0}{\partial x \partial y^2} - \frac{\partial^3 u_0}{\partial y \partial x^2} - \frac{\partial^3 u_1}{\partial y^3} + \frac{\partial T_1}{\partial x} \quad (2)$$

$$Ra_H \left\{ u_0 \frac{\partial T_0}{\partial x} + v_0 \frac{\partial T_0}{\partial y} \right\} = \frac{\partial^2 T_0}{\partial x^2} + \frac{\partial^2 T_1}{\partial y^2} \quad (3)$$

(7) proper boundary conditions

$$u_i = v_i = 0 \text{ at } y = 0 \text{ and } y = 1$$

$$\frac{\partial T_i}{\partial y} = 0 \text{ at } y = 0 \text{ and } y = 1$$

$$\int_0^1 u_i dy = 0 \text{ for mass conservation}$$

for all i

(8) Solve solutions systematically

(a)

$\frac{\partial^2 T_0}{\partial y^2} = 0 \Rightarrow T_0(x, y) = a(x)y + b(x)$ $BC \Rightarrow a(x) = 0 \Rightarrow T_0(x, y) = b(x) = T_0(x)$	$\frac{\partial^3 u_0}{\partial y^3} = \frac{\partial T_0}{\partial x} = b'$ $\Rightarrow u_0(x, y) = \frac{b'}{6}y^3 + c(x)y^2 + d(x)y + e(x)$ $BC's \Rightarrow e(x) = 0$ $\frac{b'}{6} + c + d = 0$ $\frac{b'}{24} + \frac{c}{3} + \frac{d}{2} = 0$ $\Rightarrow u_0(x, y) = b'(x) \left(\frac{y^3}{6} - \frac{y^2}{4} + \frac{y}{12} \right)$
$-\frac{\partial v_0}{\partial y} = \frac{\partial u_0}{\partial x} = b''(x) \left(\frac{y^3}{6} - \frac{y^2}{4} + \frac{y}{12} \right)$ $\Rightarrow -v_0(x, y) = b''(x) \left(\frac{y^4}{24} - \frac{y^3}{12} + \frac{y^2}{24} \right) + f(x)$ $BC's \Rightarrow f(x) = 0 \text{ and } b''(x) = 0$ $\Rightarrow v_0(x, y) = 0$ $b(x) = K_1 x + K_2$	<p>In remark:</p> $T_0(x, y) = K_1 x + K_2$ $u_0(x, y) = K_1 \left(\frac{y^3}{6} - \frac{y^2}{4} + \frac{y}{12} \right)$ $v_0(x, y) = 0$

(c) Notice that $v_0(x, y) = 0$, $u_0(x, y) = u_0(y)$ and $T_0(x, y) = T_0(x)$ linear in x . The equations are reduced to

$$\frac{\partial u_1}{\partial x} + \frac{\partial v_1}{\partial y} = 0 \quad (1)$$

$$0 = -\frac{\partial^3 u_1}{\partial y^3} + \frac{\partial T_1}{\partial x} \quad (2)$$

$$Ra_H u_0 \frac{\partial T_0}{\partial x} = \frac{\partial^2 T_1}{\partial y^2} \quad (3)$$

$\frac{\partial^2 T_1}{\partial y^2} = Ra_H u_0 \frac{\partial T_0}{\partial x} = K_1^2 Ra_H \left(\frac{y^3}{6} - \frac{y^2}{4} + \frac{y}{12} \right)$ $\Rightarrow T_1(x, y) = K_1^2 Ra_H \left(\frac{y^5}{120} - \frac{y^4}{48} + \frac{y^3}{72} \right) + a(x)y + b(x)$ $BC's \Rightarrow a(x) = 0$	$\frac{\partial^3 u_1}{\partial y^3} = \frac{\partial T_1}{\partial x} = b'(x)$ $\Rightarrow u_1(x, y) = b'(x) \left(\frac{y^3}{6} - \frac{y^2}{4} + \frac{y}{12} \right)$ <p style="text-align: center;">same as (a)</p>
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In remark:

$$T_1(x, y) = K_1^2 Ra_H \left(\frac{y^5}{120} - \frac{y^4}{48} + \frac{y^3}{72} \right) + K_3 x + K_4$$

$$u_1(x, y) = K_3 \left(\frac{y^3}{6} - \frac{y^2}{4} + \frac{y}{12} \right)$$

$$v_1(x, y) = 0$$

It turns out **the systematic solution has the same form at all orders in ϵ** . Therefore,

$$T(x, y) = K_1 x + K_2 + \left(\frac{H}{L} \right)^2 K_1^2 Ra_H \left(\frac{y^5}{120} - \frac{y^4}{48} + \frac{y^3}{72} \right)$$

$$u(x, y) = K_1 \left(\frac{y^3}{6} - \frac{y^2}{4} + \frac{y}{12} \right)$$

$$v(x, y) = 0$$

$$K_1 = C_1 + C_2 \left(\frac{H}{L} \right) + C_3 \left(\frac{H}{L} \right)^2 + \dots \quad (\text{new definitions of } K_1 \text{ and } K_2)$$

$$K_2 = C_1^* + C_2^* \left(\frac{H}{L} \right) + C_3^* \left(\frac{H}{L} \right)^2 + \dots$$

Or in dimensional form:

$$\frac{T - T_{cold}}{\Delta T} = K_1 \frac{x}{L} + K_2 + K_1^2 \left(\frac{H^2}{L^2} Ra_H \right) \left\{ \frac{1}{120} \left(\frac{y}{H} \right)^5 - \frac{1}{48} \left(\frac{y}{H} \right)^4 + \frac{1}{72} \left(\frac{y}{H} \right)^3 \right\}$$

$$\frac{u}{\alpha Ra_H / L} = K_1 \left(\frac{1}{6} \left(\frac{y}{H} \right)^3 - \frac{1}{4} \left(\frac{y}{H} \right)^2 + \frac{1}{12} \left(\frac{y}{H} \right)^3 \right)$$

$$\frac{v}{\alpha H Ra_H / L^2} = 0$$

Send regions

matching conditions: $v, \frac{\partial v}{\partial x} \rightarrow 0$ as $x \rightarrow \delta H$

boundary conditions: $u, v = 0$ at $x = 0$ and $y = 0, y = H$

(1) integral analysis

(a) momentum equation

$$\int_0^{\delta H} \int_0^H \left\{ \frac{\partial}{\partial x} \left(u \frac{\partial v}{\partial x} + v \frac{\partial v}{\partial y} \right) - \frac{\partial}{\partial y} \left(u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} \right) \right\} = v \left\{ \frac{\partial}{\partial x} \left(\frac{\partial^2 v}{\partial x^2} + \frac{\partial^2 v}{\partial y^2} \right) - \frac{\partial}{\partial y} \left(\frac{\partial^2 u}{\partial x^2} + \frac{\partial^2 u}{\partial y^2} \right) \right\} + g\beta \frac{\partial T}{\partial x} dy dx$$

Noticed that

$$u \frac{\partial v}{\partial x} \Big|_0^{\delta H} = 0 \quad \because u = 0 \text{ at } x = 0 \text{ (BC) and } \frac{\partial v}{\partial x} = 0 \text{ at } x = \delta H \text{ (MC)}$$

$$v \frac{\partial v}{\partial y} \Big|_0^{\delta H} = 0 \quad \because v = 0 \text{ at } x = 0 \text{ (BC) and } \frac{\partial v}{\partial y} = 0 \text{ at } x = \delta H \text{ (MC)}$$

$$u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} \Big|_0^H = 0 \quad \because u, v = 0 \text{ at } y = 0 \text{ and } y = H \text{ (BCs)}$$

Moreover, because of

$$\frac{\partial v}{\partial y}, \frac{\partial^2 v}{\partial y^2} = 0 \quad \text{at } x = 0 \text{ (BC) and } x = \delta H \text{ (MC)}$$

$$\frac{\partial u}{\partial x}, \frac{\partial^2 u}{\partial x^2} = 0 \quad \text{at } y = 0 \text{ and } y = H \text{ (BCs)}$$

Therefore

$$0 = \int_0^H \frac{\partial^2 v}{\partial x^2} \Big|_0^{\delta H} dy - v \int_0^{\delta H} \frac{\partial^2 u}{\partial y^2} \Big|_0^H dx + g\beta \int_0^H (T(\delta H, y) - T_{cold}) dy$$

Or in dimensionless form

$$\int_0^1 T_e(\delta, y_c) dy_c = - \int_0^1 \frac{\partial^2 v_e}{\partial x_1^2} \Big|_0^\delta dy_c + \int_0^\delta \frac{\partial^2 u_e}{\partial y_c^2} \Big|_0^1 dx$$

where

$$\begin{aligned}
u_e, v_e &\equiv u/u_e^* , v/u_e^* \\
u_e^* &\equiv g\beta H^2 \Delta T / \nu = \frac{\alpha}{H} Ra_H \\
T_e &\equiv (T - T_{cold}) / \Delta T \\
x_1 &\equiv x/H , y_c \equiv y/H
\end{aligned}$$

(b) energy equation: $\int_0^{\delta H} \int_0^H \left\{ u \frac{\partial T}{\partial x} + v \frac{\partial T}{\partial y} = \alpha \left\{ \frac{\partial^2 T}{\partial x^2} + \frac{\partial^2 T}{\partial y^2} \right\} \right\} dy dx$

Noticed that

$$vT = 0 \text{ at } y = 0 \text{ and } y = H \text{ (BCs)}$$

$$\frac{\partial T}{\partial x} \rightarrow \frac{K_1 \Delta T}{L} \text{ as } x \rightarrow \delta H \text{ (MC)}$$

$$\frac{\partial T}{\partial y} = 0 \text{ at } y = 0, y = H \text{ (BCs)}$$

Therefore

$$\int_0^H u T(\delta H) dy = \alpha \int_0^H \left\{ \frac{K_1 \Delta T}{L} - \frac{\partial T}{\partial x}(0, y) \right\} dy$$

Or in dimensionless form:

$$Ra_H \int_0^1 u_e T_e(\delta, y_c) dy_c = K_1 \frac{H}{L} - \int_0^1 \frac{\partial T_e}{\partial x_1}(0, y_c) dy_c$$

(2) Guess reasonable profiles for velocity and temperature in the end regions:

(a) x-velocity:

$$\begin{aligned}
u_e &= 0 \text{ at } y_c = 0, y_c = 1 \\
u_e &\rightarrow \frac{H}{L} u_c = K_1 \frac{H}{L} \left(\frac{y_c^3}{6} - \frac{y_c^2}{4} + \frac{y_c}{12} \right) \text{ as } x_1 \rightarrow \delta
\end{aligned}$$

$$\text{guess } u_e = K_1 \frac{H}{L} f \left(\frac{x_1}{\delta} \right) \left(\frac{y_c^3}{6} - \frac{y_c^2}{4} + \frac{y_c}{12} \right) \text{ with the following constraints on } f:$$

$$\begin{aligned}
f(0) = 0 &\Leftrightarrow u_e = 0 \text{ at } x_1 = 0 \\
f(1) = 1 &\Leftrightarrow u_e \rightarrow \frac{H}{L} u_c \text{ as } x_1 \rightarrow \delta \\
f'(0) = 0 &\Leftrightarrow v_e(0, y_c) = 0 \text{ at } x_1 = 0 + \text{continuity eqn} \\
f'(1) = 0 &\Leftrightarrow \frac{\partial u_e}{\partial x_1} = 0 \text{ as } x_1 \rightarrow \delta \\
f''(1) = 0 &\Leftrightarrow \frac{\partial^2 u_e}{\partial x_1^2} = 0 \text{ as } x_1 \rightarrow \delta
\end{aligned}$$

Thus

$$u_e = K_1 \frac{H}{L} \left(\frac{x_1}{\delta} \right)^2 \left(6 - 8 \frac{x_1}{\delta} + 3 \left(\frac{x_1}{\delta} \right)^2 \right) \left(\frac{y_c^3}{6} - \frac{y_c^2}{4} + \frac{y_c}{12} \right)$$

(b) y-velocity: from continuity equation

$$\begin{aligned}
\frac{\partial u_e}{\partial x_1} + \frac{\partial v_e}{\partial y_c} = 0 &\Rightarrow \frac{\partial v_e}{\partial y_c} = -\frac{\partial u_e}{\partial x_1} = 12 \frac{K_1}{\delta} \frac{H}{L} \frac{x_1}{\delta} \left(1 - \frac{x_1}{\delta} \right)^2 \left(\frac{y_c^3}{6} - \frac{y_c^2}{4} + \frac{y_c}{12} \right) \\
&\Rightarrow v_e = -\frac{K_1}{\delta} \frac{H}{L} \frac{x_1}{\delta} \left(1 - \frac{x_1}{\delta} \right)^2 \left(\frac{y_c^4}{2} - y_c^3 + \frac{y_c^2}{2} \right) + g(x_1)
\end{aligned}$$

boundary conditions: $v_e = 0$ at $x = 0$ and $y = 0$, $y = H \Rightarrow g(x_1) = 0$

$$v_e = -\frac{K_1}{\delta} \frac{H}{L} \frac{x_1}{\delta} \left(1 - \frac{x_1}{\delta} \right)^2 \left(\frac{y_c^4}{2} - y_c^3 + \frac{y_c^2}{2} \right)$$

(c) temperature profile:

$$T_e = 0 \text{ at } x_1 = 0$$

$$\frac{\partial T_e}{\partial y_c} = 0 \text{ at } y_c = 0, y_c = 1$$

$$T_e \Leftrightarrow T_c = K_1 x_c + K_2 + \left(\frac{K_1 H}{L} \right)^2 Ra_H \left(\frac{y^5}{120} - \frac{y^4}{48} + \frac{y^3}{72} \right) \text{ as } x_1 \rightarrow \delta$$

guess $T_e = \underbrace{\left\{ T_c(\delta, y_c) - \delta \frac{K_1 H}{L} \right\} h\left(\frac{x_1}{\delta}\right)}_{\text{correction part}} + \underbrace{\frac{K_1 H}{L} x_1}_{\text{linear part}}$ with

$$h(0) = 0 \Leftrightarrow T_e = 0 \text{ at } x_1 = 0$$

$$h(1) = 1 \Leftrightarrow T_e \rightarrow T_c(\delta, y) \text{ as } x_1 \rightarrow \delta$$

$$h'(1) = 0 \Leftrightarrow \frac{\partial T_e}{\partial x_1} \rightarrow \frac{\partial T_c}{\partial x_1} = \frac{K_1 H}{L} \text{ as } x_1 \rightarrow \delta$$

Consequently,

$$T_e = \underbrace{\left\{ T_c(\delta, y_c) - \delta \frac{K_1 H}{L} \right\}}_{\text{correction part}} \left(2 \frac{x_1}{\delta} - \left(\frac{x_1}{\delta} \right)^2 \right) + \underbrace{\frac{K_1 H}{L} x_1}_{\text{linear part}}$$

(3) results: substitute (2) into (1):

$$K_2 + \frac{\delta H K_1}{L} + \frac{H^2 K_1^2 R a_H}{1440 L^2} = \frac{H K_1}{10 \delta^3 L} + \frac{3 \delta H K_1}{5 L}$$

$$- \left(\frac{H K_1}{L} \right)^3 \frac{R a_H^2}{362880} = \frac{H K_1}{L} - \left\{ \frac{2 K_2}{\delta} + \frac{H K_1}{L} + \left(\frac{H K_1}{L} \right)^2 \frac{R a_H}{720 \delta} \right\}$$

after rearrangement:

$$K_2 + \left(\frac{H K_1}{L} \right)^2 \frac{R a_H}{1440} = \frac{2 \delta H K_1}{5 L} \left(\frac{1}{4 \delta^4} - 1 \right)$$

$$\left(\frac{H K_1}{L} \right)^3 \frac{\delta R a_H^2}{725760} = K_2 + \left(\frac{H K_1}{L} \right)^2 \frac{R a_H}{1440}$$

two equations for three unknowns: K_1 , K_2 , δ for given values of $\frac{H}{L}$ and $R a_H$.

(4) third equation: Noticed that the flow is symmetric about the geometric center of the cavity. Thus

$$T_c = \frac{1}{2} \quad \text{at} \quad x_c = \frac{1}{2} \quad \text{and} \quad y_c = \frac{1}{2}$$

i.e.

$$\frac{K_1}{2} + K_2 + \left(K_1 \frac{H}{L} \right)^2 \frac{R a_H}{1440} = \frac{1}{2}$$

(5) solve the system of algebraic equations: define

$$\Omega \equiv K_2 + \left(\frac{H K_1}{L} \right)^2 \frac{R a_H}{1440}$$

and rewrite equations as follows

$$\Omega = \frac{2\delta HK_1}{5L} \left(\frac{1}{4\delta^4} - 1 \right) = \delta \left\{ \left(\frac{HK_1}{L} \right)^3 \frac{Ra_H^2}{725760} \right\} = \frac{1}{2} - \frac{K_1}{2}$$

thus

$$(a) \quad \delta = \left\{ \left(\frac{HK_1}{L} \right)^3 \frac{Ra_H^2}{725760} \right\}^{-1} \left(\frac{1}{2} - \frac{K_1}{2} \right)$$

$$(b) \quad \frac{2\delta HK_1}{5L} \left(\frac{1}{4\delta^4} - 1 \right) = \frac{1}{2} - \frac{K_1}{2}$$

$$(c) \quad \Omega = K_2 + \left(\frac{HK_1}{L} \right)^2 \frac{Ra_H}{1440} = \frac{1}{2} - \frac{K_1}{2}$$

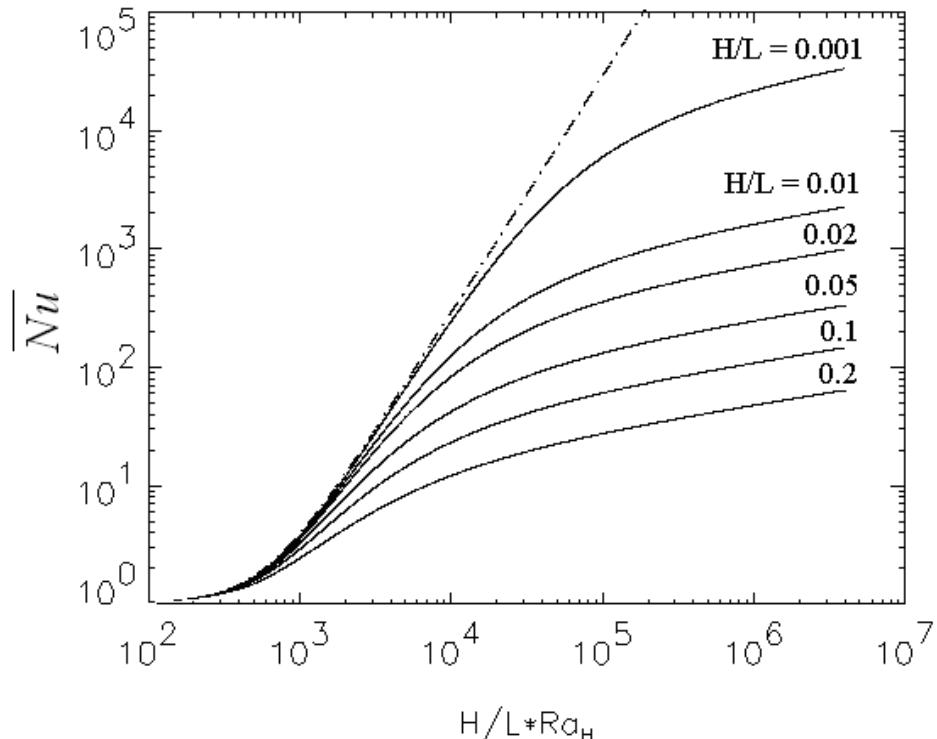
\Rightarrow given $\frac{H}{L}$ and Ra_H \Rightarrow find K_1 by root-searching (b) with δ replaced by (a)

(6) The conduction-referenced Nusselt number:

$$q' \equiv k \int_{-H/2}^{H/2} \left(-\frac{\partial T}{\partial x} \right)_{x=0} dy$$

$$\overline{Nu} \equiv \frac{q'}{(kH\Delta T)/L} = K_1 + \frac{K_1^3}{362880} \left(\frac{H}{L} Ra_H^2 \right)^2$$

(in terms of dimensional variables)



$$1. \quad T_c(\delta, y_c) = \frac{K_1 \delta H}{L} + K_2 + \left(\frac{K_1 H}{L} \right)^2 Ra_H \left(\frac{y_c^5}{120} - \frac{y_c^4}{48} + \frac{y_c^3}{72} \right)$$

$$2. \quad T_e = \left\{ T_c(\delta, y_c) - \delta \frac{K_1 H}{L} \right\} \left(2 \frac{x_1}{\delta} - \left(\frac{x_1}{\delta} \right)^2 \right) + \frac{K_1 H}{L} x_1$$

$$3. \quad \left(\frac{\partial T_e}{\partial x_1} \right)_{x_1=0} = \left\{ T_c(\delta, y_c) - \delta \frac{K_1 H}{L} \right\} \frac{2}{\delta} + \frac{K_1 H}{L} = \frac{2T_c(\delta, y_c)}{\delta} - \frac{K_1 H}{L}$$

$$= \frac{K_1 H}{L} + \frac{2K_2}{\delta} + \frac{2}{\delta} \left(\frac{K_1 H}{L} \right)^2 Ra_H \left(\frac{y_c^5}{120} - \frac{y_c^4}{48} + \frac{y_c^3}{72} \right)$$

$$4. \quad \int_{-1/2}^{1/2} \left(\frac{\partial T_e}{\partial x_1} \right)_{x_1=0} dy_c = \int_{-1/2}^{1/2} \left\{ \frac{K_1 H}{L} + \frac{2K_2}{\delta} + \frac{2}{\delta} \left(\frac{K_1 H}{L} \right)^2 Ra_H \left(\frac{y_c^5}{120} - \frac{y_c^4}{48} + \frac{y_c^3}{72} \right) \right\} dy_c$$

$$= \frac{K_1 H}{L} + \frac{2K_2}{\delta} - \frac{1}{3840\delta} \left(\frac{K_1 H}{L} \right)^2 Ra_H$$

$$5. \quad q' \equiv k \int_{-H/2}^{H/2} \left(-\frac{\partial T}{\partial x} \right)_{x=0} dy = k \Delta T \int_{-1/2}^{1/2} \left(-\frac{\partial T_e}{\partial x_1} \right)_{x_1=0} dy_c$$

$$6. \quad \overline{Nu} \equiv \frac{q'}{(kH\Delta T)/L} = \frac{k \Delta T \left\{ \frac{K_1 H}{L} + \frac{2K_2}{\delta} - \frac{1}{3840\delta} \left(\frac{K_1 H}{L} \right)^2 Ra_H \right\}}{(kH\Delta T)/L}$$

$$= K_1 + \frac{2L}{\delta H} \left\{ K_2 - \frac{1}{7680} \left(\frac{K_1 H}{L} \right)^2 Ra_H \right\}$$

$$= K_1 + \frac{2L}{\delta H} \left\{ \frac{1-K_1}{2} - \left(\frac{K_1 H}{L} \right)^2 \frac{Ra_H}{1440} - \frac{1}{7680} \left(\frac{K_1 H}{L} \right)^2 Ra_H \right\}$$

$$= K_1 + \frac{2L}{\delta H} \left\{ \frac{1-K_1}{2} - \frac{19}{23040} \left(\frac{K_1 H}{L} \right)^2 Ra_H \right\}$$

$$= K_1 + 2 \left\{ \left(\frac{H}{L} \right)^2 K_1^3 \frac{Ra_H^2}{725760} \right\} \left\{ 1 - \frac{38}{23040} \frac{1}{1-K_1} \left(\frac{K_1 H}{L} \right)^2 Ra_H \right\}$$

$$\cong K_1 + \frac{K_1^3}{362880} \left(\frac{H}{L} Ra_H^2 \right)^2$$